

# Performance Optimization of Hybrid Steam-Solvent (Huff-n-Puff) Processes in a Post-CHOPS Reservoir

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## Problem Statement

Cold Heavy Oil Production with Sand (CHOPS) usually leaves the reservoir with about 85-90% of its OOIP. Implementation of the hybrid steam-solvent processes can improve mobility and increase oil recovery.

## Objectives

The goal of this project is to evaluate the performance of the hybrid steam-solvent processes, determine which co-injected solvent mixture will optimize production and examine its effects on the huff-n-puff method.

## Methodology

- Data collection from IHS AccuMap & AccuLog, and literature.
- Development a 3D reservoir geological model with CMG Builder.
- Material balance (MB) calculation to determine average reservoir pressure.
- Perform history matching with MBE and sand production history by CMG CMOST-AI.
- Evaluate performance of the best scenario of the hybrid steam-solvent processes.
- Examine the effect of variable time setting from sensitivity analysis.
- Perform economic analysis for the hybrid steam-solvent process.

## Acknowledgments

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## References

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Yang, S., Fan, Z., & Yang, D. (2020). A modified Pressure-gradient-based (PGB) sand Failure criterion for dynamically and preferentially characterizing WORMHOLE growth and propagation During Chops processes. *Journal of Petroleum Science and Engineering*, 192, 107250. doi:10.1016/j.petrol.2020.107250

## Design Process

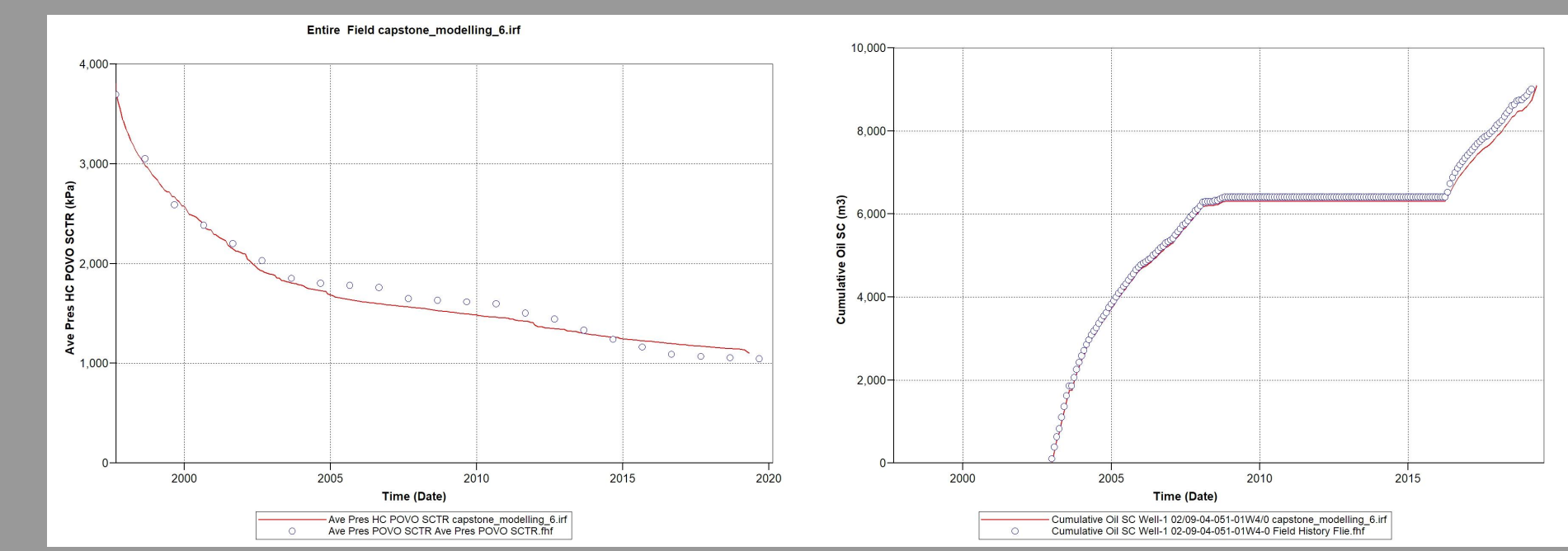


Figure 4: Reservoir Pressure History Match(left) and Oil Production History Match (right)

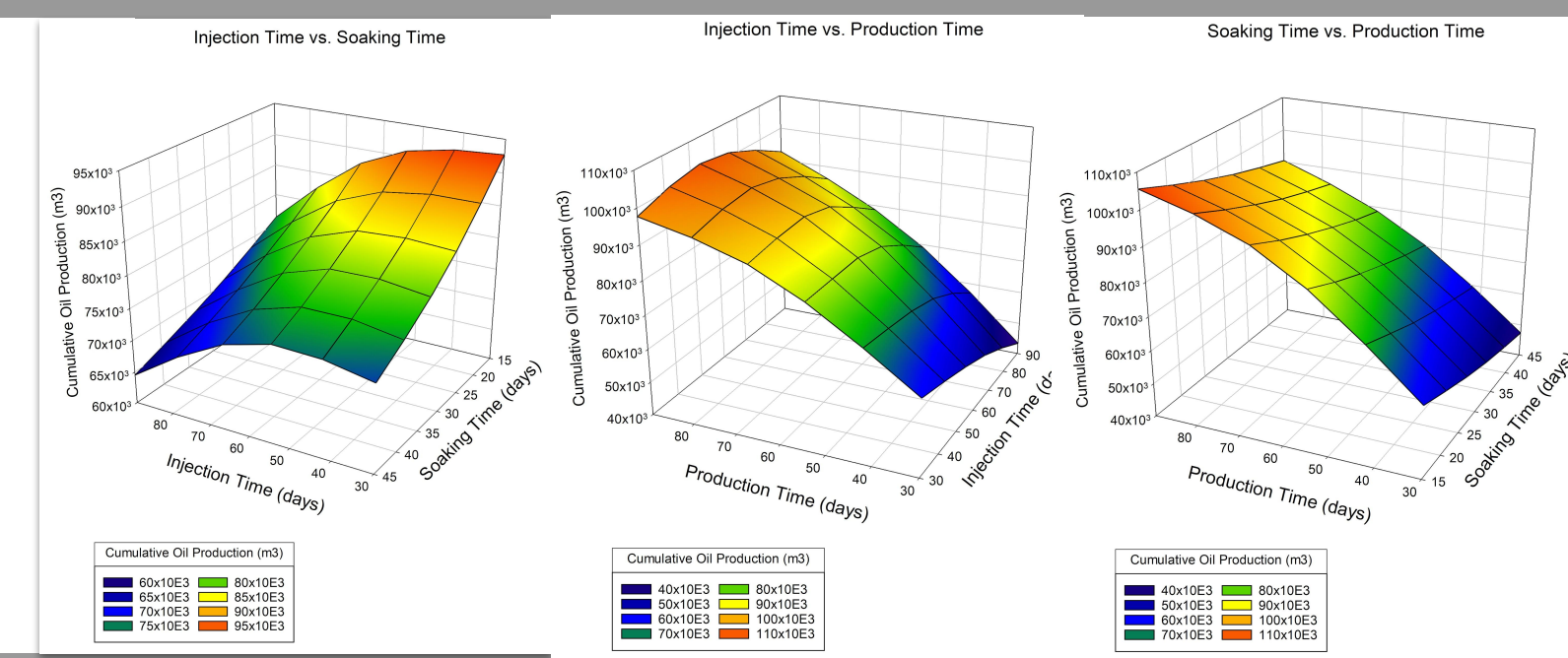


Figure 7: 3D plots with injection time, soaking time, and production time vs. cumulative oil production

Table 1: Thirteen scenarios for 10-year performance prediction in a Post CHOPS reservoir

Scenario No.	Compositions of the injected fluids
#1	100.0 mol% CO <sub>2</sub>
#2	100.0 mol% flue gas
#3	5.0 mol% C <sub>3</sub> H <sub>8</sub> - 5.0 mol% n-C <sub>4</sub> H <sub>10</sub> - 90.0 mol% CO <sub>2</sub>
#4	5.0 mol% C <sub>3</sub> H <sub>8</sub> - 5.0 mol% n-C <sub>4</sub> H <sub>10</sub> - 90.0 mol% flue gas
#5	100.0 mol% steam
#6	90.0 mol% CO <sub>2</sub> - 10.0 mol% steam
#7	90.0 mol% flue gas - 10.0 mol% steam
#8	4.5 mol% C <sub>3</sub> H <sub>8</sub> - 4.5 mol% n-C <sub>4</sub> H <sub>10</sub> - 81.0 mol% CO <sub>2</sub> - 10.0 mol% steam
#9	4.5 mol% C <sub>3</sub> H <sub>8</sub> - 4.5 mol% n-C <sub>4</sub> H <sub>10</sub> - 81.0 mol% flue gas - 10.0 mol% steam
#10	10.0 mol% CO <sub>2</sub> - 90.0 mol% steam
#11	10.0 mol% flue gas - 90.0 mol% steam
#12	0.5 mol% C <sub>3</sub> H <sub>8</sub> - 0.5 mol% n-C <sub>4</sub> H <sub>10</sub> - 9.0 mol% CO <sub>2</sub> - 90.0 mol% steam
#13	0.5 mol% C <sub>3</sub> H <sub>8</sub> - 0.5 mol% n-C <sub>4</sub> H <sub>10</sub> - 9.0 mol% flue gas - 90.0 mol% steam

## Field Background

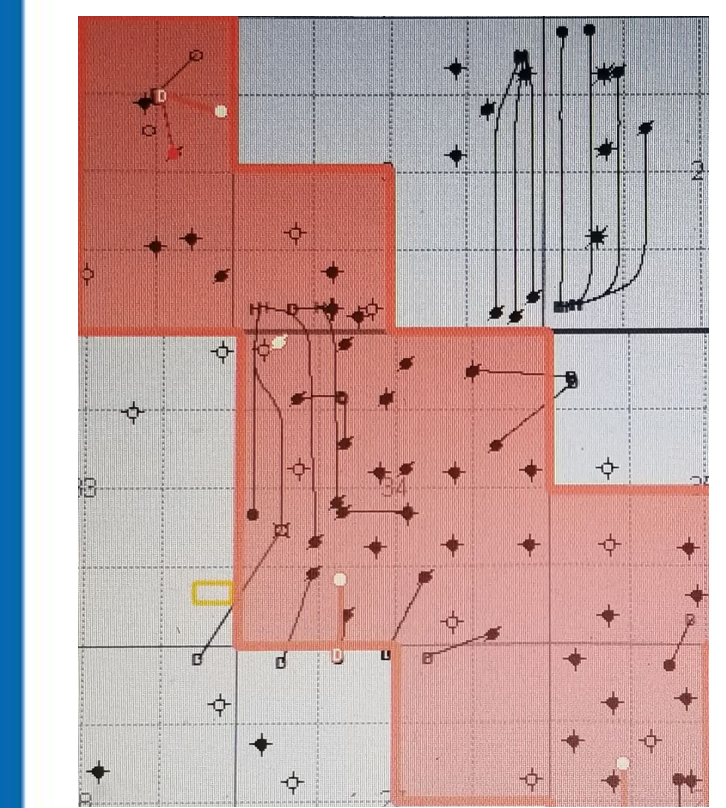


Figure 1: Field Map (Retrieved from AccuMap)

Table 2: Properties of Lloydminster CHOPS reservoir used in the simulation model

Reservoir Properties	Value
Well Location	C0/12-26-050-01W4/0
Depth to reservoir top (m)	550
Net pay (m)	4.69
Porosity	0.31
Oil saturation	0.75
Horizontal rock permeability kh (mD)	581.14
k <sub>v</sub> /k <sub>h</sub>	0.1
Effective rock compressibility (1/kPa)	0.0000485
Reference pressure (kPa)	3703
Initial reservoir temperature	22
Reference depth (m)	730

## MBE Modification

The material balance equation is used to calculate the average reservoir pressure over time. (See Figure 2)

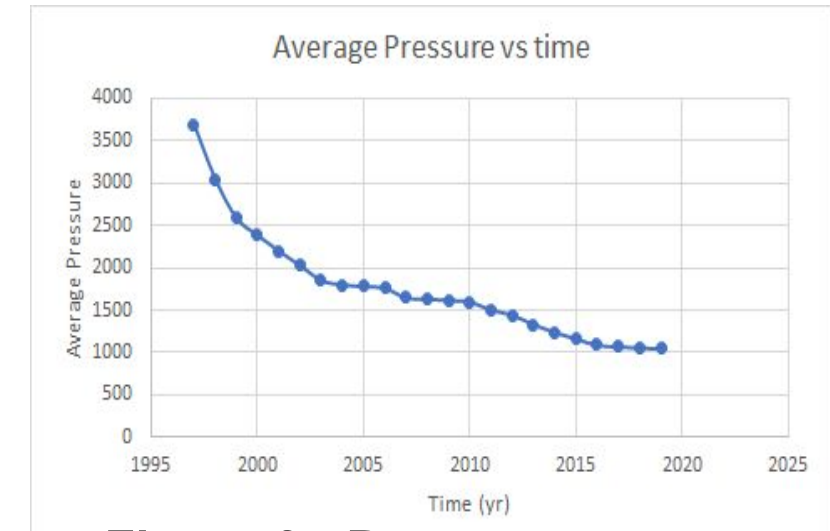


Figure 2: Pressure curve calculated from MBE

## Reservoir Modelling

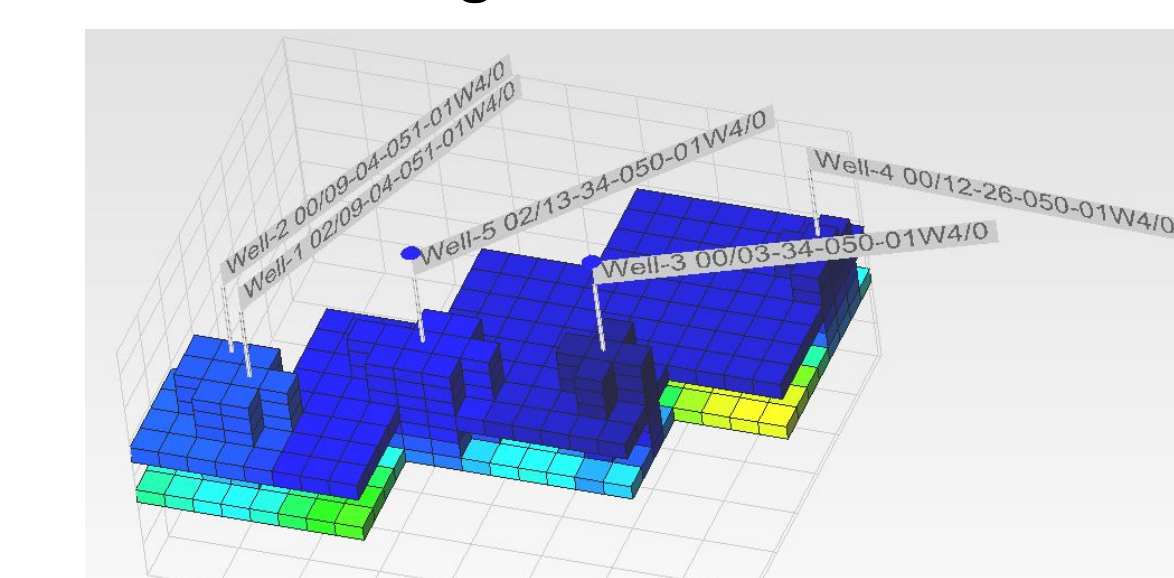


Figure 3: Reservoir model from Heavy Oil Post-CHOPS reservoir in the West Lloydminster Field and 3D model map

## History Matching

- The reservoir pressure matches at a global error of 3% with production rate as an input constraints.
- The simulated sand production of well UWI 02-13-34-050-01W4/0 only has 5% error.
- Oil production profile were perfectly matched from 1997 to 2019 profiles for 5 wells.

## Performance Evaluation

With 351 data retrieved from CMG STARS thermal recovery simulator, the most optimal case is the 100 mol% of flue gas injection with injection period in 60 days; soaking period in 45 days and production period in 90 days

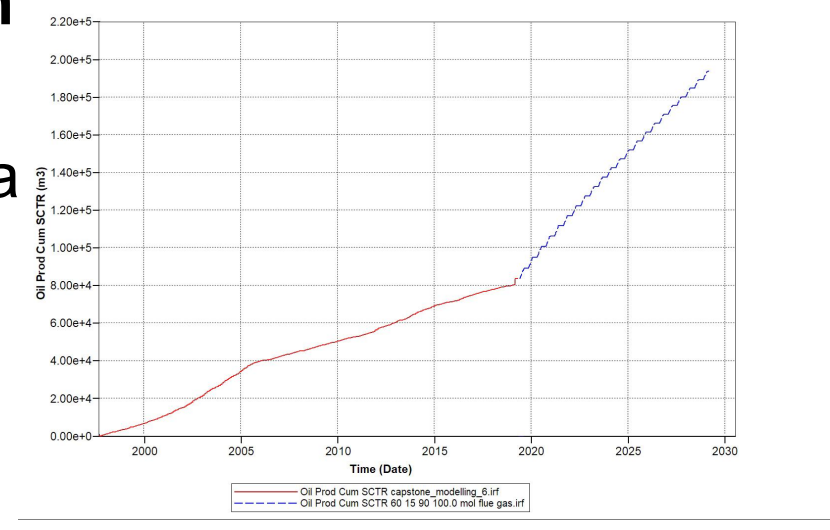


Figure 5: 10-year CSS performance prediction in a Post CHOPS reservoir with 100%mol flue gas injection method

## Wormhole Generation

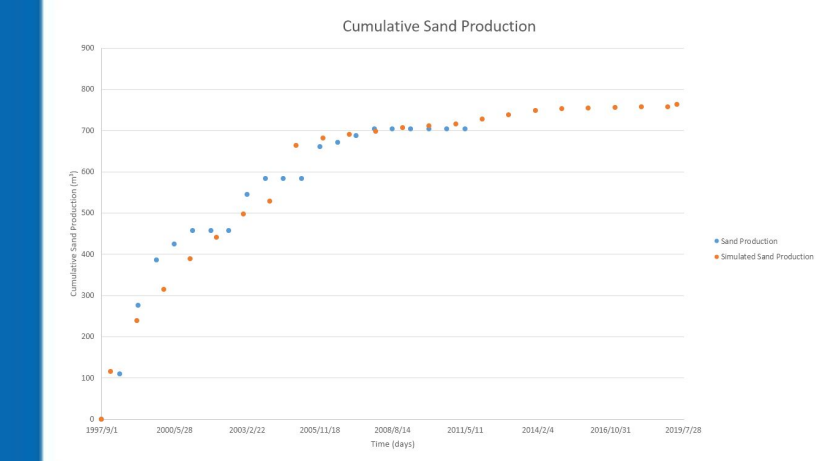


Figure 6: Sand Production History Match

## Sensitivity Analysis

With the results from Figure 7 & 8, it can be concluded that the optimal case will be:

- A moderate injection time (60 days).
- A shorter injection time (15 days).
- A longer injection time (90 days).

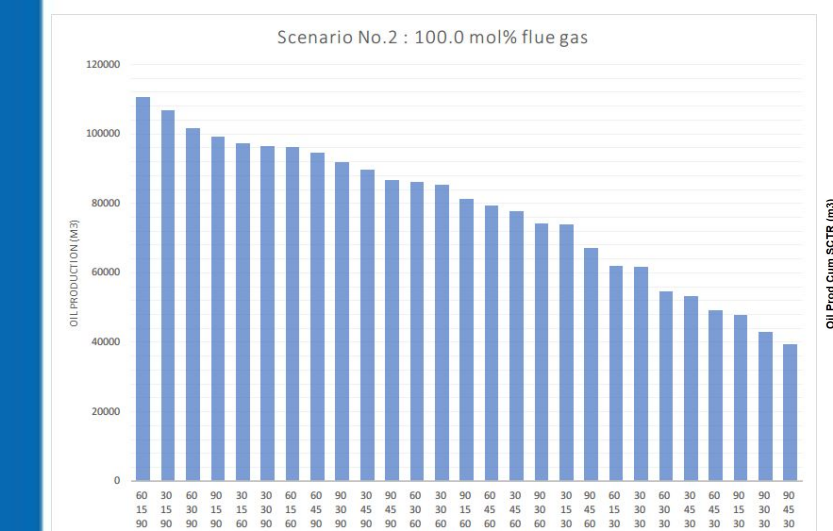


Figure 8: Cumulative oil production vs. different time setting for 100 mol% flue gas

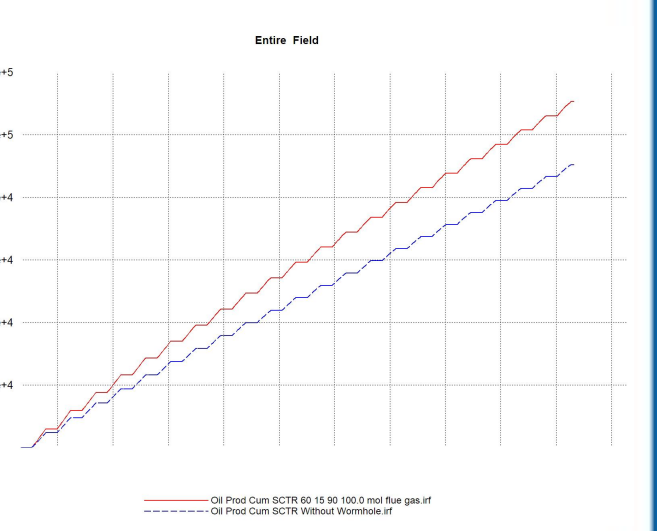
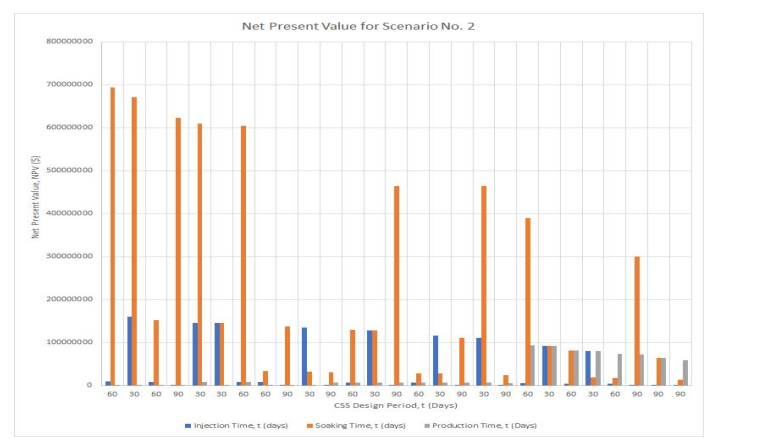


Figure 9: Wormhole Effect Comparison

## Economic Analysis

- Using the 13 scenarios stated in Table 1, a Net Present Value (NPV) plot is generated for each scenario. The aim is to determine which scenario will achieve the highest NPV during a 10 year performance evaluation in a Post-CHOPS reservoir.
- The results show that Scenario #2 (100 mol% flue gas) gives the highest NPV value.

Figure 10: Net Present Value Calculation Results for scenario #2



## Conclusions

- The optimal case for the steam-solvent injection in a post-CHOPS reservoir is 100 mol% flue gas and steam which produces an additional 1.1E6 cubic meters of oil during a ten year period.
- The wormhole network included in the geological model increases oil recovery under various hybrid steam-solvent processes.